

**Tikrit University**

**The College of Petroleum Processes Engineering**

**Petroleum Systems Control Engineering**

**Department**

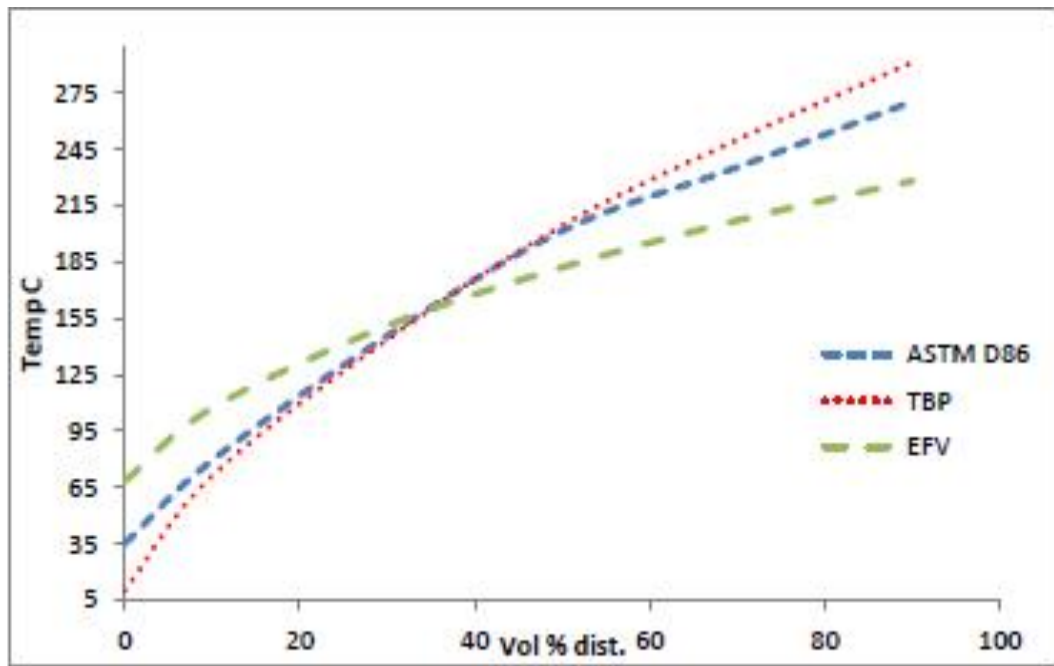
**Properties of Petroleum & Natural Gas**

**Third Class**

**Lecture 13**

**By**

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**Figures**

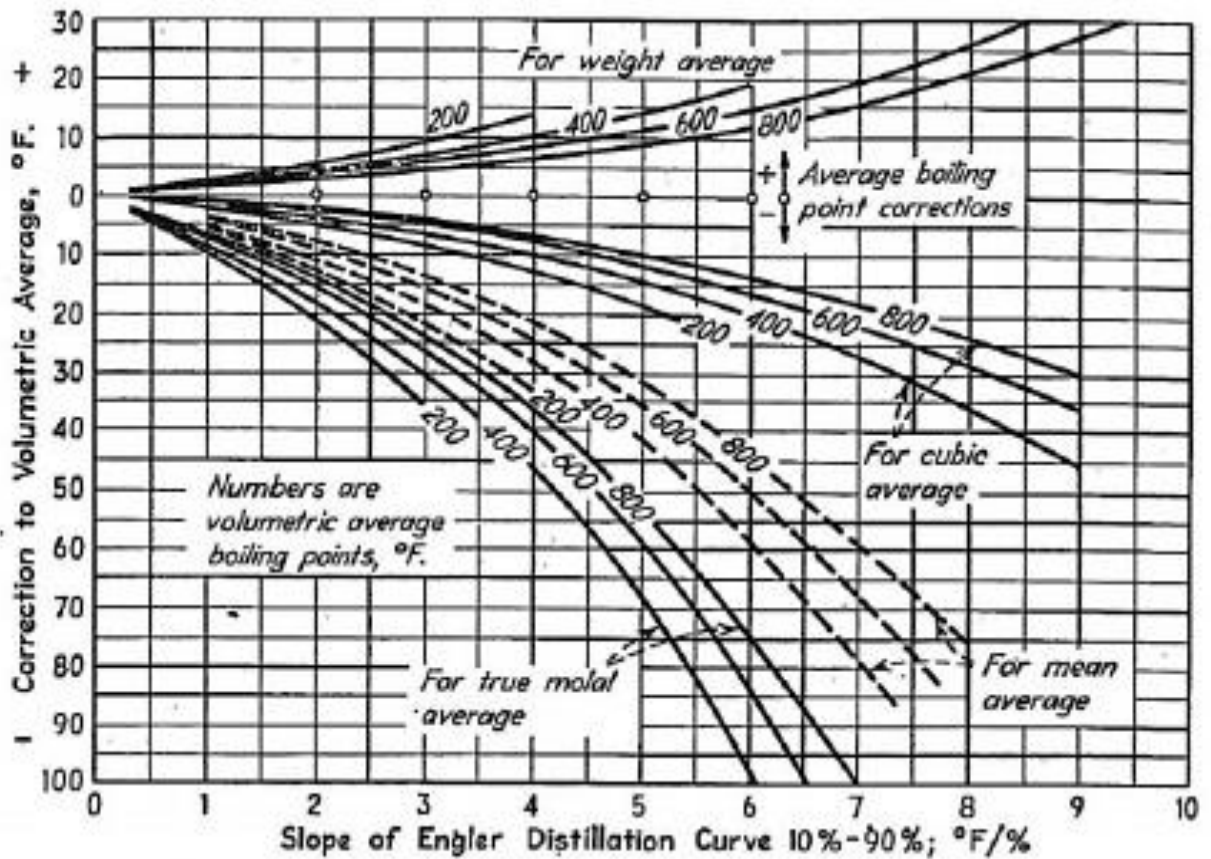


Figure (1): Characterizing Boiling Points of Petroleum Fractions

Q4: The ASTM D86 data of crude oil fraction having specific gravity of 0.720 at 60/60 °F is shown below.

Vol % distilled	IBP	5	10	30	50	70	90	95	EP
ASTM D86 °C	37	42	49	66	93	133	203	211	217

- Calculate VABP, also find MeABP and WABP from Figure 1.
- Find the molecular weight of the fraction and compare with the value obtained from Figure 2.
- Find the base of the fraction.
- Give suitable name for the fraction.

### Solution

a)

$$VABP = \frac{120.2 + 150.8 + 199.4 + 271.4 + 397.4}{5} = 227.84 \text{ } ^\circ\text{F}$$

$$SL = \frac{397.4 - 120.2}{90 - 10} = 3.465 \text{ } ^\circ\text{F}$$

Refer to Figure 1. Read down from a slope of 3.465°F to the interpolated curve to 227.84 °F in the set drawn with dashed lines (MeABP). Read a correction value of -25 on the ordinate. Then find MeABP from equation below. Do the same for WABP, then read a correction of +10.

$$MeABP = 227.84 \text{ } ^\circ\text{F} - 25 \text{ } ^\circ\text{F} = 203.84 \text{ } ^\circ\text{F}$$

$$WABP = 227.84 \text{ } ^\circ\text{F} + 10 \text{ } ^\circ\text{F} = 238.84 \text{ } ^\circ\text{F}$$

b)

$$Tb = \frac{T30 + T50 + T70}{3} = \frac{66 + 93 + 133}{3} = 97.33 = 370.48$$

M =

$$42.965[\exp(2.097 \times 10^{-4} T_b - 7.7812SG + 2.08476 \times 10^{-3} T_b SG)] T_b^{1.26007} SG^{4.98300} = 100.264$$

c)

$$kw = \frac{\sqrt{MeABP R}}{SG} = 12.11 \text{ paraffinic base}$$

d) The name of the fraction is Gasoline

The API of the fraction from the calculation for gravity is 65. Using Figure (2) and the MeABP obtained from Figure (1.A), a molecular weight of 100 is read off.

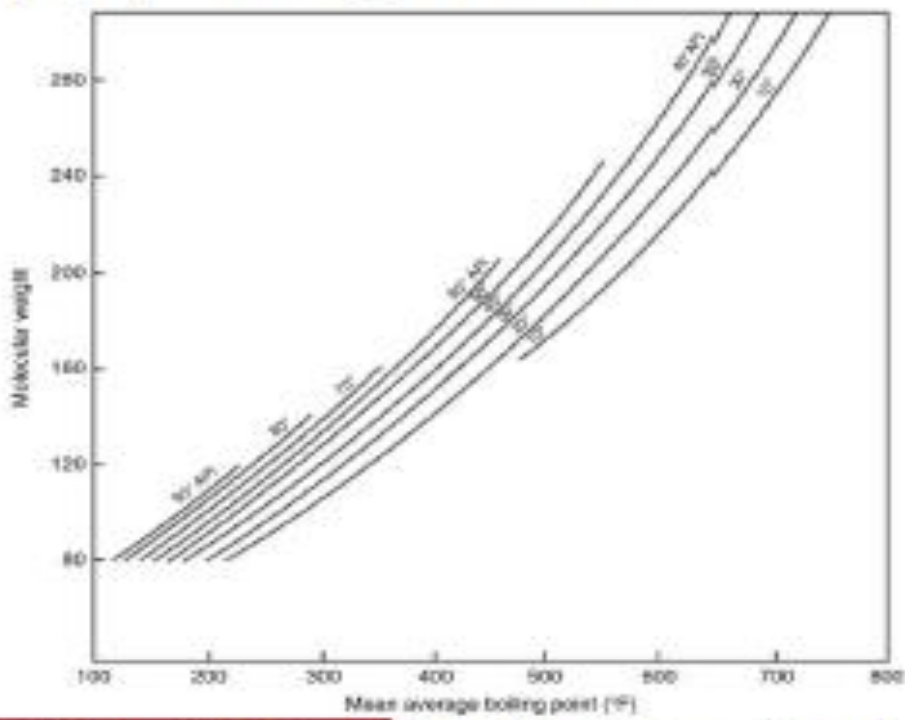


Figure (2): Correlation between boiling point, molecular weight, and gravity

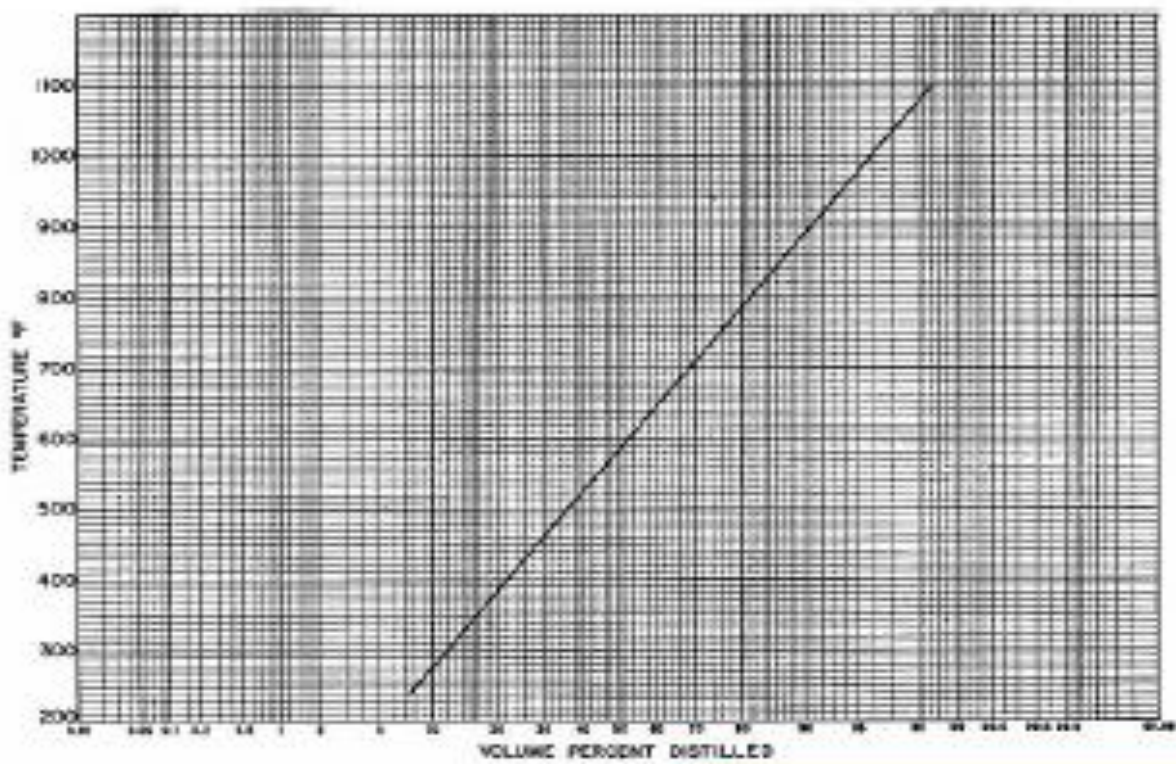


Figure (3): Crude distillation curve

Example: Consider the petroleum cut has 197-222 °C (387-432 °F) boiling range for the curve given in Figure (3).

Step 1: Volumetric range: According to the Figure (3), the volumetric range corresponding to these cuts is 20-25 i.e. vol % distilled of the fraction is 5% vol. This gives us directly the volumetric flowrate of this fraction, that is, a 5% of the total flowrate

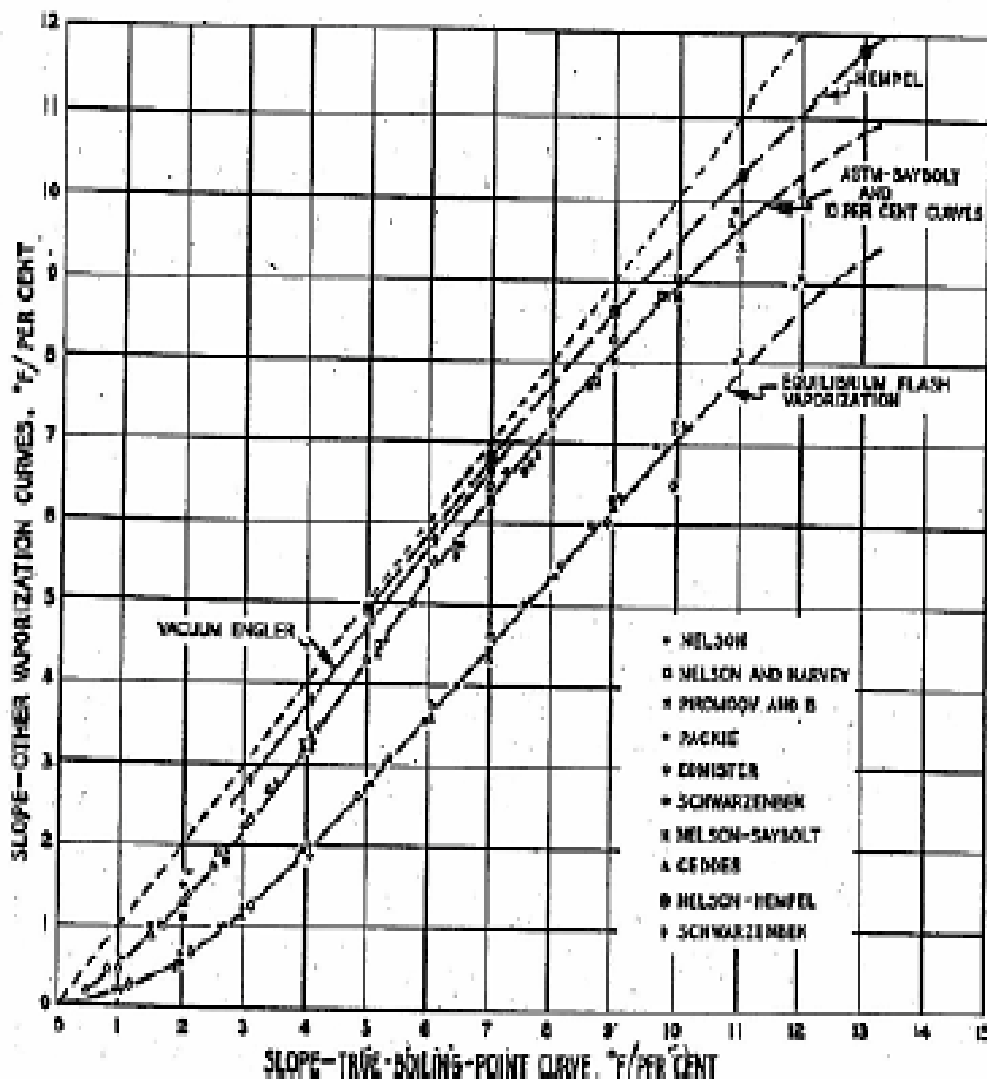


Figure (4): Relationships between the slopes of various distillation curves

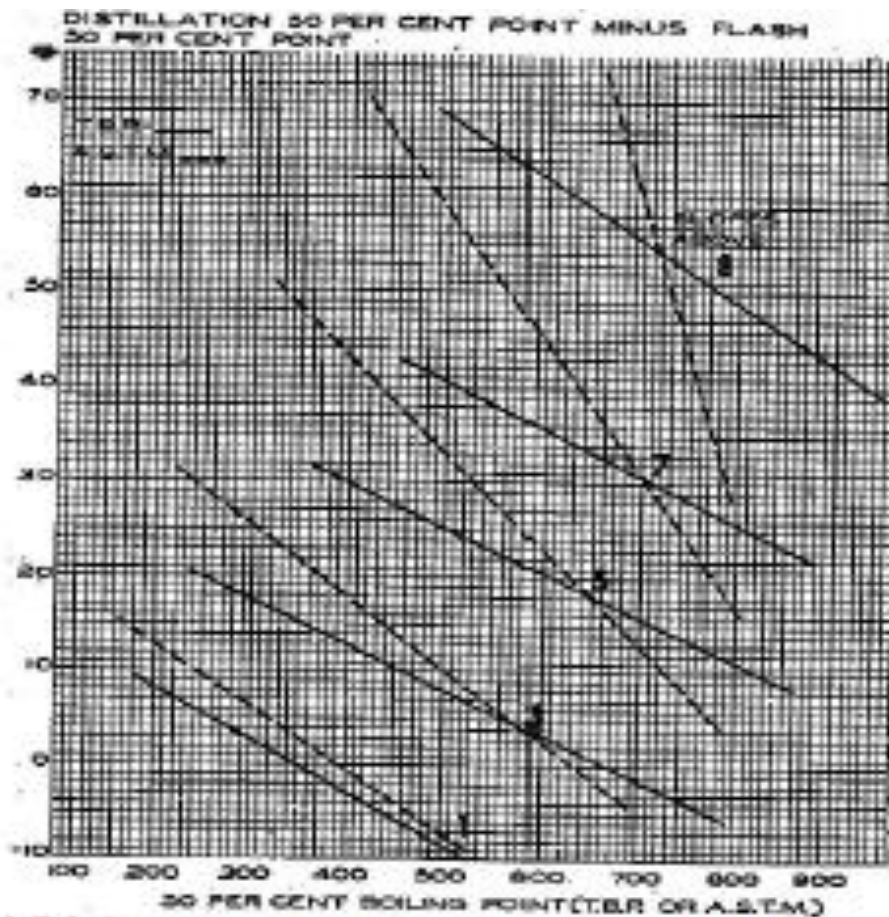


Figure (5) Relationships between distillation temperatures at 50% vaporized and the flash (E.F.V.) Temp. at 50% vol vaporized

Q5: Find  $T_{100\%}$  and  $T_0$  for EFV curve knowing that TBP ( $T_{50\%} = 570^\circ\text{F}$ ) and Slope =  $9.4^\circ\text{F}$

Solution

Step 1: find the EVF slope from Figure 4.

$$SL(\text{EFV}) = 6.5^\circ\text{F}$$

Step 2: find  $T_{50\%}$  for EFV curve from TBP ( $T_{50\%} = 570^\circ\text{F}$ ) using Figure 5.

The  $T_{50\%}$  of the flash curve will be about  $64^\circ\text{F}$  below the  $T_{50\%}$  of the TBP curve

$$T_{50\% \text{ EFV}} = 570 - 64 = 506^\circ\text{F}$$

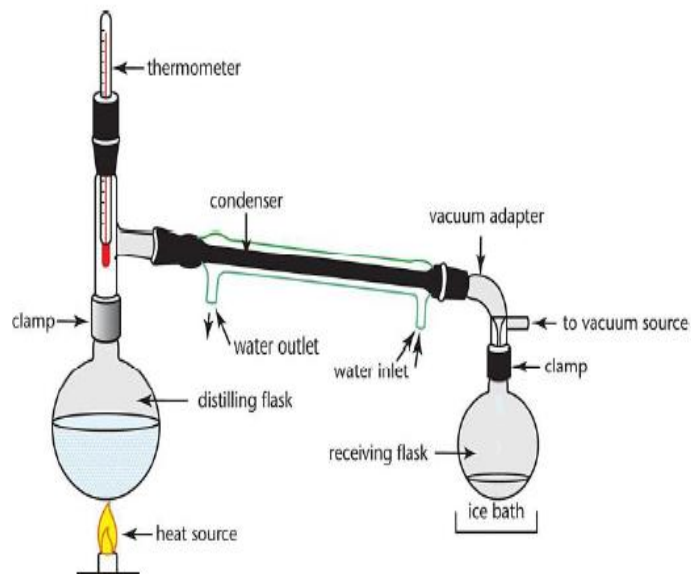
Step 3:

$$6.5 = \frac{T_{100} - 506}{50 - 0} \rightarrow T_{100} = 831^\circ\text{F}$$

$$6.5 = \frac{506 - T_0}{100 - 50} \rightarrow T_0 = 181^\circ\text{F}$$

## ASTM D1160

- Boiling point ranges of heavy petroleum fractions such as products of a vacuum distillation column cannot be measured due to the thermal decomposition of heavy hydrocarbons at high temperatures.
- For this reason distillation data are performed at reduced pressures of 1-50 mmHg, as described under ASTM D 1160 test method.
- In this part we present calculation methods for the conversion of ASTM D 1160 to atmospheric distillation curve and for the prediction of atmospheric TBP curves from ASTM D 1160.



ASTM D1160 apparatus diagram

Conversion of a Boiling Point at Sub- or Super-Atmospheric Pressures to the Normal Boiling Point or Vice Versa.

$$T'_b(760 \text{ mmHg}) = \frac{748.1 QT}{1 + T(0.3861Q - 0.00051606)} \dots 1$$

**Equation 1** is used to convert boiling point at sub-atmospheric ( $P < 760$  mm Hg) or super-atmospheric ( $P > 760$  mm Hg) conditions to normal boiling point.

$$Q = \frac{6.761560 - 0.987672 \log_{10} P}{3000.538 - 43 \log_{10} P} \quad (P < 2 \text{ mm Hg})$$

$$Q = \frac{5.994296 - 0.972546 \log_{10} P}{2663.129 - 95.76 \log_{10} P} \quad (2 \leq P \leq 760 \text{ mm Hg})$$

$$Q = \frac{6.412631 - 0.989679 \log_{10} P}{2770.085 - 36 \log_{10} P} \quad (P > 760 \text{ mm Hg})$$

Where  $P$  = pressure at which boiling point or distillation data is available, mm Hg.

$T$  = boiling point available at given pressure  $P$ , in kelvin.

$T_b$  = normal atmospheric boiling point, in kelvin.

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At  $P = 10$  mmHg,  $Q = 0.001956$  and as a result **Eq. (1)** reduces to the following simple form:

$$T(10\text{mmHg}) = \frac{0.683398 T'_b}{1 - 1.63434 \times 10^{-4} T'_b} \dots\dots 2$$

- To use equations (1,2) for the conversion of boiling point from one low pressure to another low pressure (i.e., from 1 to 10 mm Hg), two steps are required.
- In the first step, normal boiling point or  $T$  (760 mm Hg) is calculated from  $T$  (1 mmHg) by Eq. (1) and in the second step  $T$  (10 mm Hg) is calculated from  $T$  (760 mm Hg) or  $T_b$  via Eq. (2).