**Tikrit University**

# **The College of Petroleum Processes Engineering Petroleum Systems Control Engineering Department**

**Properties of Petroleum & Natural Gas** 

**Third Class**

**Lecture 10**

**By**

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## **Average Boiling Points**

- $\overline{\text{■}}$  Boiling points of petroleum fractions are presented by distillation curves such as ASTM D86 or TBP.
- $\pm$  In prediction of physical properties and characterization of hydrocarbon mixtures a single characteristic boiling point is required.
- Average boiling point for a fraction is defined to determine the single characterizing boiling point.
- $\pm$  There are five average boiling points defined by the following equations. Three of these average boiling points are VABP (volume average boiling point), MABP (molal average boiling point) and WABP (weight average boiling point), defined for a mixture of n components as

$$
ABP = \sum_{i=1}^{n} x_i T_{bi}
$$

- Where **ABP** is the VABP, MABP, or WABP and *xi* is the corresponding volume, mole, or weight fraction of component i. **Tbi** is the normal boiling point of component **i in kelvin**.
- Two other average boiling points are CABP (cubic average boiling point) and MeABP (mean average boiling point) defined as

$$
MeABP = \frac{MABP + CABP}{2}
$$

For petroleum fractions in which volume, weight, or mole fractions of components are not known, the average boiling points are calculated through ASTM D 86 distillation curve as

$$
VABP = \frac{T_{10} + T_{30} + T_{50} + T_{70} + T_{90}}{5}
$$

Where  $T_{10}$ ,  $T_{30}$ ,  $T_{50}$ ,  $T_{70}$ , and  $T_{90}$  are ASTM temperatures at 10, 30, 50, 70, and 90 vol% distilled.

#### **Slope of the ASTM distillation curves**

 $\overline{A}$  A parameter that approximately characterizes slope of a distillation curve is the slope of a linear line between 10 and 90% points. This slope shown by SL is defined as

$$
SL = \frac{T_{90} - T_{10}}{90 - 10}
$$

- When the boiling points of compounds are near each other the value **of SL and the boiling range of the fraction are low.**
- **For heavy fractions and vacuum distillates in which distillation data by ASTM D1160 are available, they should first be converted to ASTM D 86 and then average boiling points are calculated.**
- Analytical correlations for estimation of average boiling points are given by the following equations in terms of VABP and SL.

 $ABP = VABP - \Delta T$  $WABP = VABP - \Delta T_W$  $MABP = VABP - \Delta T_M$  $\mathbf{C}ABP = \mathbf{V}ABP - \Delta T_c$  $\boldsymbol{MeABP} = \boldsymbol{VABP} - \Delta \boldsymbol{T}_{\boldsymbol{Me}}$ 

Where ABP is an average boiling point such as WABP, MABP, CABP, or MeABP and ΔT is the corresponding correction temperature for each ABP. **All temperatures are in kelvin**.

 $\ln(-\Delta T_w) = -3.64991 - 0.02706(VABP - 273.15)^{0.6667} + 5.163875 SL^{0.25}$  $\ln(\Delta T_M) = -1.15158 - 0.01181(VABP - 273.15)^{0.6667} + 3.70612 SL^{0.333}$  $\ln(\Delta T_c) = -0.82368 - 0.08997(VABP - 273.15)^{0.45} + 2.456791 SL^{0.45}$  $\ln(\Delta T_{Me}) = -1.53181 - 0.0128(VABP - 273.15)^{0.6667} + 3.646064 SL^{0.33}$ 

The most useful type of ABP is MeABP, which is recommended for correlation of most physical properties as well as calculation of Watson K.

For calculation of specific heat, VABP is recommended.

**Q1:** For the straight run SR Naphtha fraction, the experimental ASTM D86 data with 98.8% recovery vol% are given below. Calculate VABP, WABP, CABP, MABP, and MeABP. Find the base of the fraction by Kw method.



**Solution:** 

$$
VABP = \frac{128 + 164 + 198 + 230 + 262}{5} = 196.4 \text{ }^{\circ}\text{F} = 91.33 \text{ }^{\circ}\text{C} = 364.48 \text{ kelvin}
$$
\n
$$
SL = \frac{127.77 - 53.33}{90 - 10} = 0.9305 \text{ }^{\circ}\text{C}
$$

 $\ln(-\Delta T_w) = -3.64991 - 0.02706(364.48 - 273.15)^{0.6667} + 5.163875 * 0.9305^{0.25}$  $\ln(\Delta T_M) = -1.15158 - 0.01181(364.48 - 273.15)^{0.6667} + 3.70612 * 0.9305^{0.333}$  $\ln(\Delta T_c) = -0.82368 - 0.08997(364.48 - 273.15)^{0.45} + 2.456791 * 0.9305^{0.45}$  $\ln(\Delta T_{Me}) = -1.53181 - 0.0128(364.48 - 273.15)^{0.6667} + 3.646064 * 0.9305^{0.33}$ 



If specific gravity of a fraction is not available, it may be estimated from available distillation curves at 10 and 50% points as given by the following equation:

 $SG = a[(T_{10})^b(T_{50})^c]$ 

where constants *a, b,* and *c* for the three types of distillation data, namely, ASTM D 86, TBP, and EFV, are given in the Table below. Temperatures at **10 and 50% are both in kelvin**.



$$
SG = 0.08342[(326.37)^{0.10731}(365.37)^{0.26288}] = 0.7323
$$

$$
K_w = \frac{\sqrt[3]{645.828 R}}{0.7323 \text{ @ } 60^{\circ}F} = 11.80
$$

## **Mean average boiling point of petroleum fractions**

Based on our experience, for narrow boiling range fractions **with SL < 0.8 °C the MeABP is very close to T<sup>50</sup> temperature in ASTM D86.** 

DIFFERENTIAL, °F



## **Types of Distillation Curve**

- **1- True Boiling point(TBP) Distillation**
- **2- ASTM Distillation**
- **3- Semi-fractionating Distillation**
- **4- Equilibrium Flash Vaporization(EFV)**

**1) TBP:** This type of distillation is commonly used due to the accuracy of the results obtained by this method which is very close to that obtained via real distillation or industrial distillation. In this distillation, there is a fractionation column located between the condenser and the flask. In general, this type of distillation is carried out by two steps: firstly, under atmospheric pressure until 300°C (1% distilled very 2 min), secondly under vacuum pressure (to prevent cracking process and to reduce the boiling point) at 40mmHg (1% distilled every 3-5 min). In this process, the vapor press. temp. is plotted vs. distilled(%) to get TBP curve.

**2) ASTM:** In this type of distillation there is on fractionation column located between the condenser and the flask. On the other hand, the raised vapor will not be fractionated in this process. This distillation is used with fractions having short range of the boiling point.

**3) Semi-fractionating distillation:** In this type of distillation, their will be some fractionating process on the raised vapor via package located between the condenser and the flask.

**4) Equilibrium Flash Vaporization (EFV):** Is a single stage separation technique. A liquid mixture feed is pumped through a heater to raise the temperature and enthalpy of the mixture. It then flows through a valve and the pressure is reduced, causing the liquid to partially vaporize. Because the vapor and liquid are in such close contact up until the "flash" occurs, the product liquid and vapor phases approach equilibrium.