

**Density and Specific Gravity ASTM D 287-92@60 °F (15.5 °C) and 1 atm.**

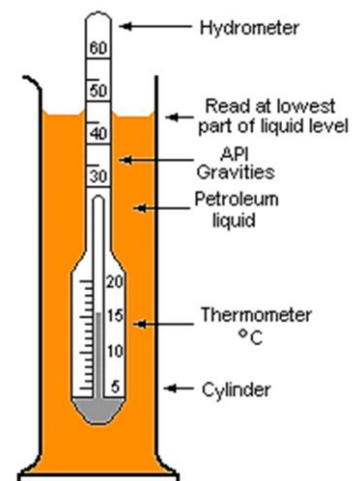
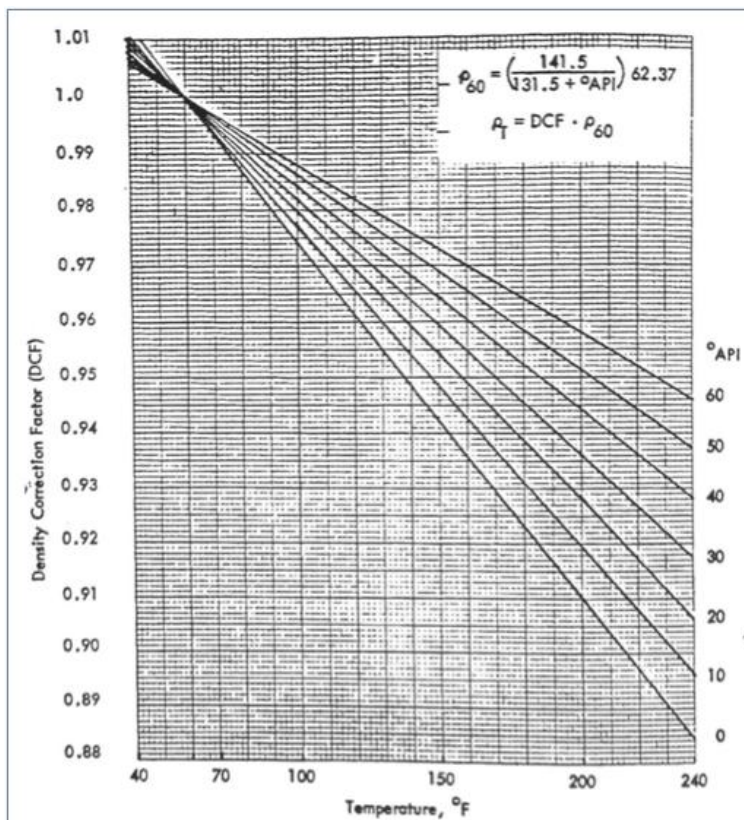
$$SG @ 60^{\circ}F = \frac{\rho \text{ of liquid at } T}{\rho \text{ of water at } T} \quad (1)$$

$$SG @ 60^{\circ}F = \frac{\rho \text{ of petroleum at } 60^{\circ}F \text{ g/cm}^3}{0.999 \frac{g}{cm^3}} \quad (2)$$

**ASTM D 287-92: API of crude oil and petroleum products by hydrometer method.**

- A hydrometer (a calibrated floating device) is placed in the sample at the specified temperature.
- The depth to which the hydrometer sinks and comes to rest in the liquid indicates the relative weight of the liquid.
- The hydrometer reading (API) is converted to specific gravity at 15.6°C or API gravity at 60°F using standard tables or figures.

$$API = \frac{141.5}{Sp. Gr. @ 60^{\circ}F} - 131.5 \dots (3)$$

**Coefficient of thermal expansion  $\gamma$** 

$$SG_{60} = SG_T + [0.000331(T(^{\circ}F) - 60)] \quad (4)$$

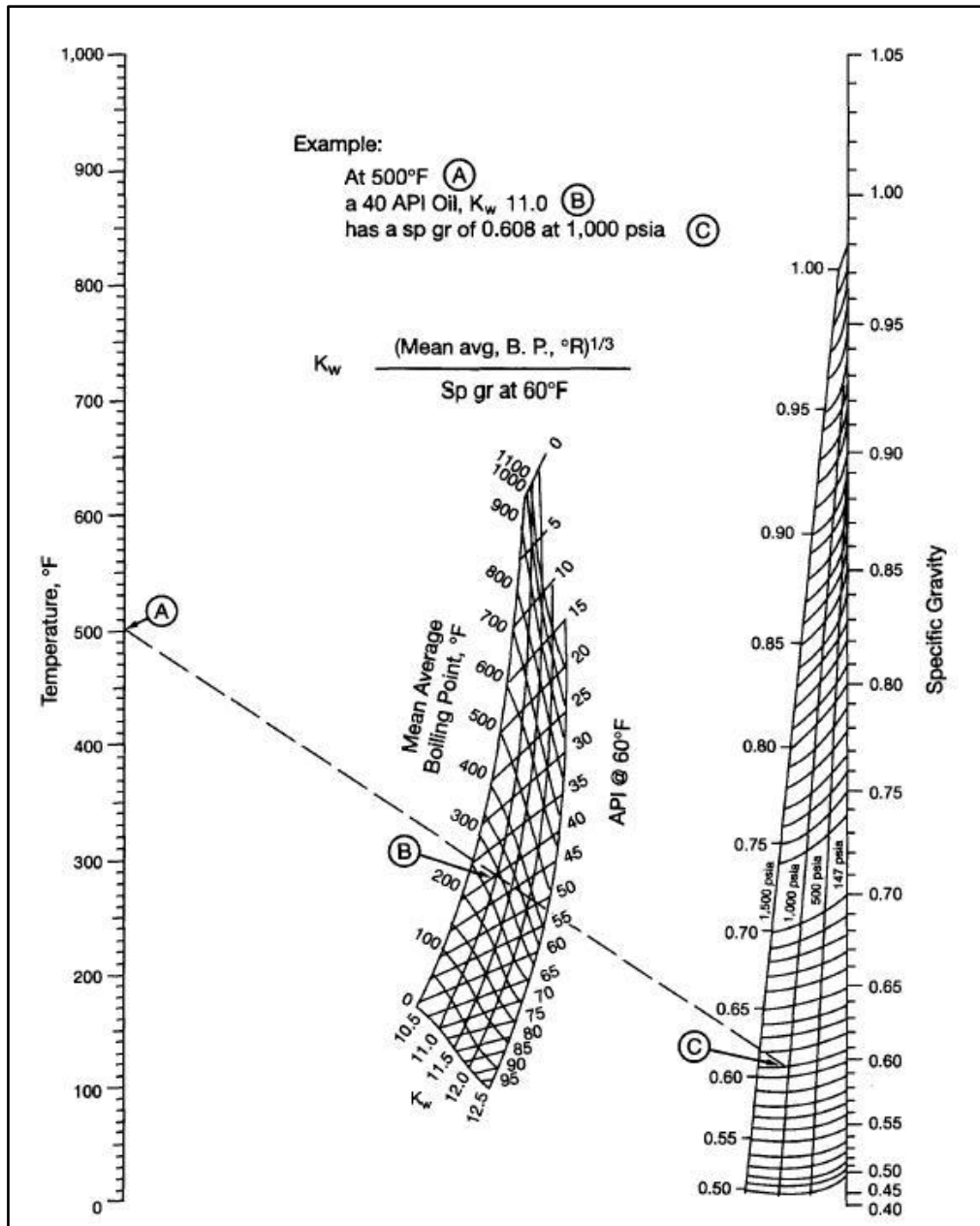
**Density at 20°C  $d_{20}$** 

$$d_{20} = 0.995 SG \dots (5)$$

Equation 5 was developed for hydrocarbons **from C<sub>5</sub> to C<sub>20</sub>**; however, it can be safely used up to C<sub>40</sub> with **PRD (percent relative deviation) of less than 0.1%**.

$$\%D = \frac{\text{estimated value} - \text{actual value}}{\text{actual value}} \times 100 \dots (6)$$

**Specific gravity of petroleum fractions as a function to K<sub>w</sub>, API, MeABP and temperature**



**Figure (1): Correlation between MeABP, K<sub>w</sub>, API and specific gravity**

**Riazi-Daubert Methods**

For **heavier fractions** (molecular weight **from 200 to 800**) the following relation in terms of kinematic viscosities developed by Riazi and Daubert may be used.

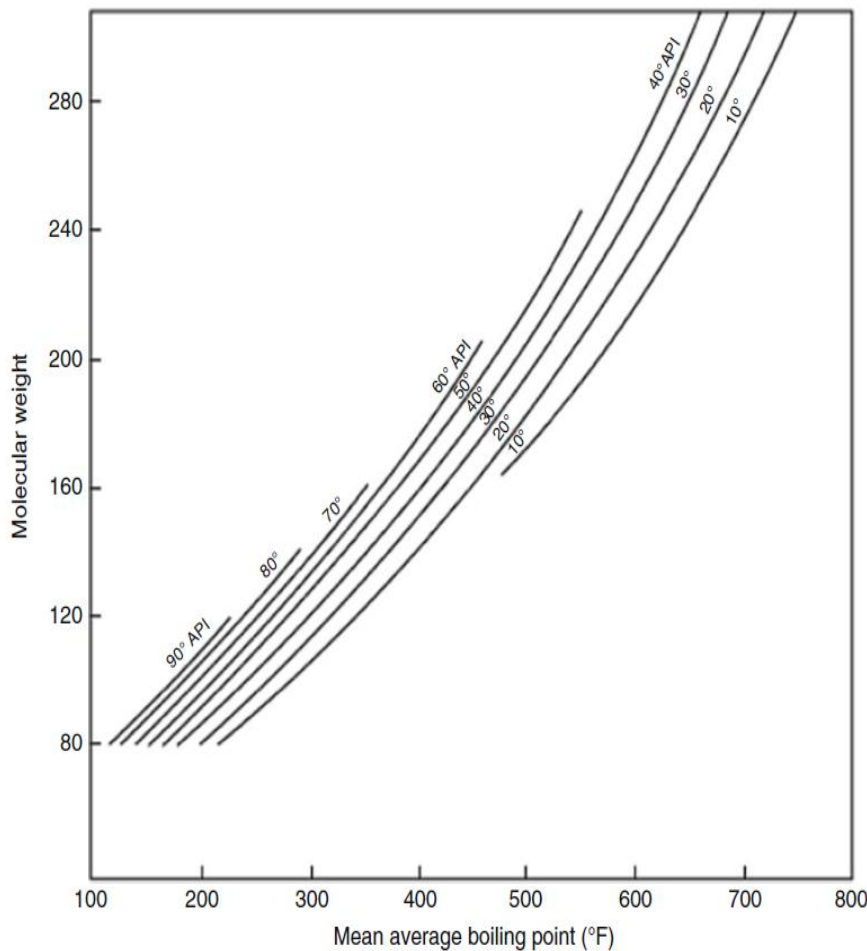
$$SG = 0.7717[v_{38}^{0.1157}][v_{99}^{-0.1616}] \quad (7)$$

**Predication of Molecular Weight (Riazi-Daubert Methods)**

- Most oil fractions have molecular weights in the range of **100-700**.

$$M = 42.965[\exp(2.097 \times 10^{-4} T_b - 7.7812SG + 2.08476 \times 10^{-3} T_b SG)]T_b^{1.26007} SG^{4.98308}$$

- Where M is the molecular weight of the petroleum fraction, **T<sub>b</sub>** is the **mean average** boiling point of the petroleum **fraction in K**, and SG is the specific gravity at 60°F.



**Figure (2): Correlation between boiling point, molecular weight, and API gravity**

- For heavy petroleum fractions, Riazi and Daubert developed a three-parameter correlation in terms of **kinematic viscosity based on the molecular** weight of heavy fractions in the range of **200-800**: the equation below is only **recommended when the boiling point is not available**.

$$M = 223.56[v_{38}^{-1.2435+1.228SG} v_{99}^{3.4758-3.038SG}]SG^{-0.6665} \quad (9)$$

A graphical presentation of Equation (9) is shown in Figure below:

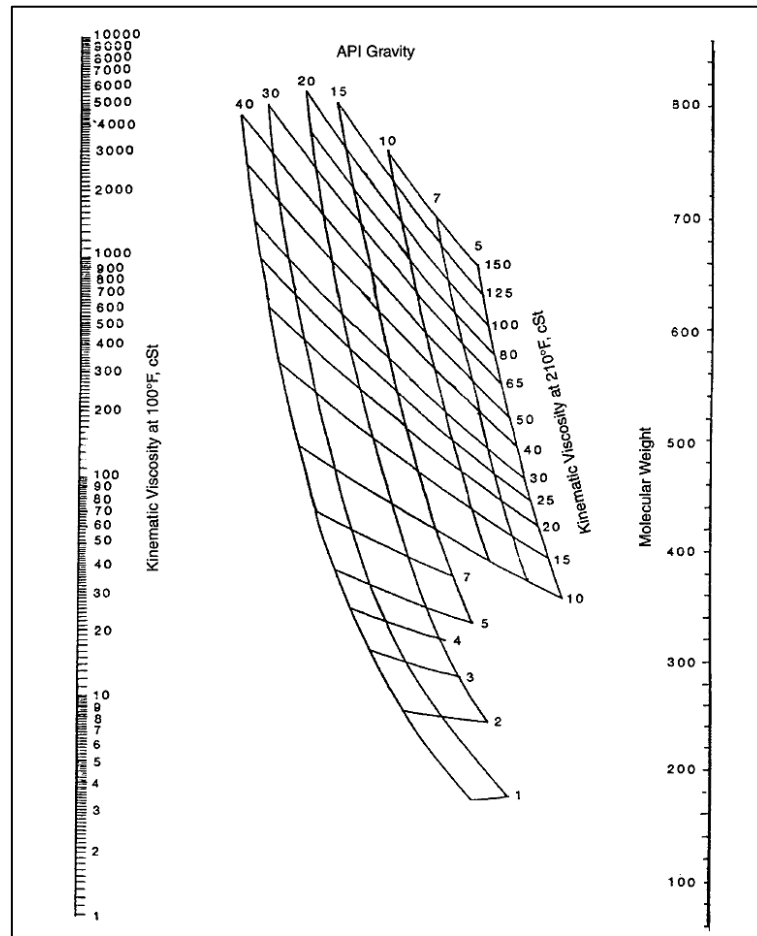


Figure (3): Correlation between viscosity, molecular weight, and gravity

#### Prediction Average Boiling Points by Riazi-Daubert Correlations

- Boiling points of petroleum fractions are presented by distillation curves such as ASTM D86 or TBP.
- There are five average boiling points:
- VABP (volume average boiling point)
- MABP (molal average boiling point)
- WABP (weight average boiling point)

$$ABP = \sum_{i=1}^n x_i T_{bi}$$

where **ABP** is the VABP, MABP, or WABP and  $x_i$  is the corresponding volume, mole, or weight fraction of component  $i$ .  $T_{bi}$  is the normal boiling point of component  $i$  in kelvin.

- CABP (cubic average boiling point)
- MeABP (mean average boiling point)

$$MeABP = \frac{MABP + CABP}{2} \quad (10)$$

For petroleum fractions in which volume, weight, or mole fractions of components are not known, the average boiling points are calculated through ASTM D 86 distillation curve as

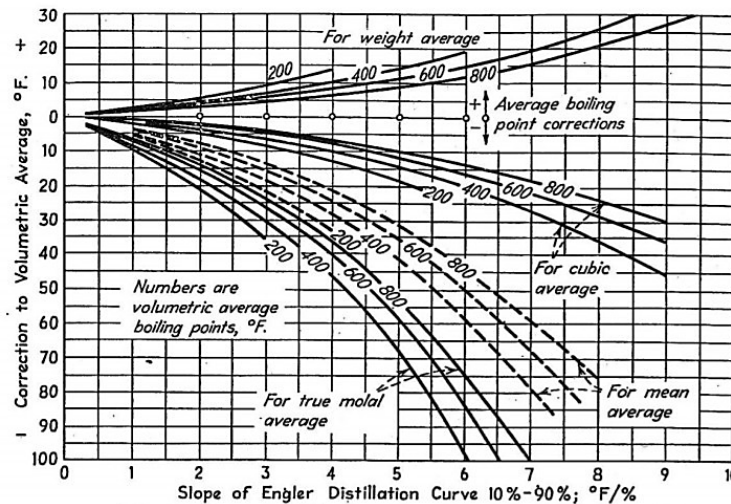
$$VABP = \frac{T_{10} + T_{30} + T_{50} + T_{70} + T_{90}}{5} \quad (11)$$

Where  $T_{10}$ ,  $T_{30}$ ,  $T_{50}$ ,  $T_{70}$ , and  $T_{90}$  are ASTM D86 temperatures at 10, 30, 50, 70, and 90 vol% distilled.

### Slope of the ASTM distillation curves

A parameter that approximately characterizes slope of a distillation curve is the slope of a linear line between 10 and 90% points. This slope shown by SL is defined as

$$SL = \frac{T_{90} - T_{10}}{90 - 10} \quad (12)$$



**Figure (4): Average Boiling Points of Petroleum Fractions**

$$ABP = VABP \pm \Delta T \quad (13)$$

$$WABP = VABP \pm \Delta T_W$$

$$MABP = VABP \pm \Delta T_M$$

$$CABP = VABP \pm \Delta T_C$$

$$MeABP = VABP \pm \Delta T_{Me}$$

$\Delta T$  is the correction temperature to **VABP** for each ABP. All temperatures are in °F.

- The most useful is **MeABP**, which is recommended for most physical properties as well as calculation of **Watson K**.

**Exercise:** For the straight run SR Naphtha fraction, the experimental **ASTM D86** data with 98.8% recovery vol% are given below. Calculate **VABP**, **WABP**, **CABP**, **MABP**, and **MeABP**. Find the base of the fraction by Kw method.

Vol% Distilled	IBP	5	10	30	50	70	90	95	FBP
ASTM D86 °F	92	118	128	164	198	230	262	272	300

**Solution:**

$$VABP = \frac{128 + 164 + 198 + 230 + 262}{5} = 196.4^{\circ}\text{F}$$

$$SL = \frac{262 - 128}{90 - 10} = 1.675^{\circ}\text{F}$$

$$\Delta T_W = +5^{\circ}\text{F} \quad WABP = 201.4^{\circ}\text{F}$$

$$\Delta T_M = -15^{\circ}\text{F} \quad MABP = 181.4^{\circ}\text{F}$$

$$\Delta T_C = -3 \quad CABP = 193.4^{\circ}\text{F}$$

$$\Delta T_{Me} = -5^{\circ}\text{F} \quad MeABP = 191.4^{\circ}\text{F}$$

**(MeABP can be calculated by eq. 10)**

If specific gravity of a fraction is not available, it may be estimated from available distillation curves at 10 and 50% points as given by the following equation:

$$SG = a[(T_{10})^b(T_{50})^c] \quad (14)$$

where constants  $a$ ,  $b$ , and  $c$  for the three types of distillation data, namely, ASTM D 86, TBP, and EFV, are given in the Table below. Temperatures at **10 and 50% are both in kelvin**.

Distillation type	$T_{10}$ range, °C	$T_{50}$ range, °C	SG range	$a$	$b$	$c$
ASTM D 86	35–295	60–365	0.70–1.00	0.08342	0.10731	0.26288
TBP	10–295	55–320	0.67–0.97	0.10431	0.12550	0.20862
EFV	79–350	105–365	0.74–0.91	0.09138	–0.0153	0.36844

$$SG = 0.08342[(326.37)^{0.10731}(365.37)^{0.26288}] = 0.7323$$

$$K_w = \frac{\sqrt[3]{651.07 R}}{0.7323 @ 60^{\circ}\text{F}} = 11.840 \text{ mixed (pf\&N)}$$

Note: To use **Figure 3**, based on the value of  $V_{38}$  a point is determined on the vertical line, then from  $V_{99}$  and  $SG$ , another points on the chart is specified. A line that connects these two points intersects with the **line of molecular weight** where it may be read as the estimated value.